

# Spectrograph design for POLLUX: preliminary estimations

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## Problem statement

- POLLUX is a high-resolution UV spectropolarimeter for the future LUVOIR large space telescope with the following target parameters

Parameter	Target value	Top goal	Comment
Shortest wavelength	98 nm	90 nm	
Longest wavelength	390 nm	visible	
Spectral resolution	120000	200000	
Aperture size	0.03"	0.01"	$y_{\text{slit}}=45 \text{ um}$
Telescope F/#	20	-	NA=0.025
Entrance pupil diameter	15 m	-	
Sampling	2.5-3 pix per resolution element	-	$\beta=0.413$ $y_{\text{slit}}'=18 \text{ um}$
Spectral length in the shortest image line	6 nm	-	

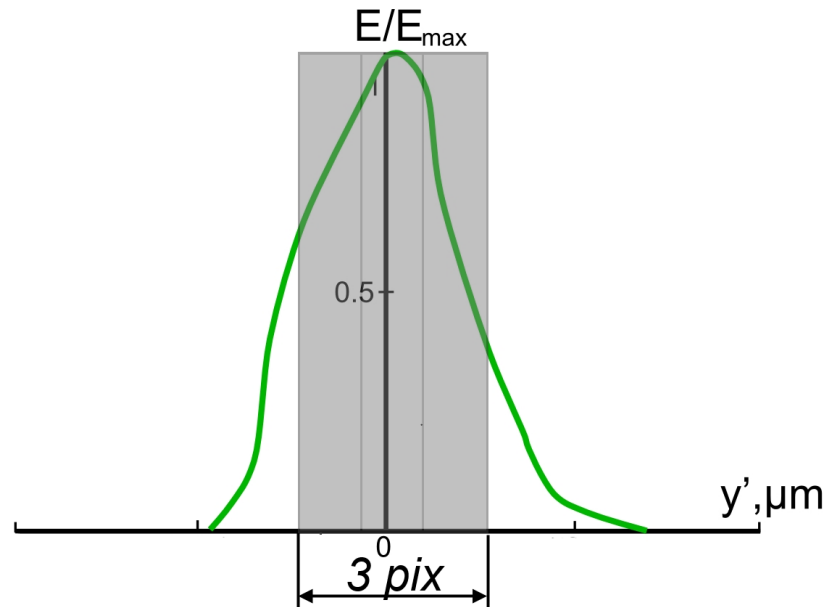


## Conceptual/principal assumptions (I)

- On the current stage the spectrograph is considered separately from the polarimeter
- It's supposed to be a multi-channel echelle spectrograph with following parameters of the channels (*see presentation by Sebastien Vives, @ this workshop*)
  - 1<sup>st</sup> (FUV) channel - 90-120nm,
  - 2<sup>nd</sup> (MUV) channel - 120-220nm,
  - 3<sup>rd</sup> (NUV) channel - 220-400nm.
- The channels uses similar optical designs with minor changes. All the design concepts and estimations are demonstrated on the example of the 2<sup>nd</sup> channel
- The design uses the minimum possible number of optical surfaces in order to increase the throughput:
  - OAP mirror as the collimator,
  - Echelle grating,
  - Single reflective grating as the cross-disperser.

## Conceptual/principal assumptions (II)

- The previous assumptions implies that the optical system is limited by aberrations (at least for a part of the working range).
  - So the spectral resolution value used for analytical computation should be higher than the target value, i.e. the collimated beam diameter and/or echelle AOI is intendenly increased.
  - Possible alternative is a higher energy concentration in the spot due to use of additional surfaces



Typical instrument function of the spectrograph



## Technological assumptions

- The detectors have the following parameters (or higher)
  - 90-120nm and 120-220nm is registered with MCPs of about 100x100mm. Pixel size is 6  $\mu\text{m}$ .
  - 220-400nm is registered with CCD of about 4kx4k (13  $\mu\text{m}$  pixel).
  - Mosaic designs are possible
  - Increase of one dimension or curving is possible for the MCP detector
  
- “Technologically safe” parameters for the echelle are
  - Grooves frequency <100 gr/mm
  - AOI <80°.
  
- Camera mirror and the cross-disperser represents a single element, which has the following features
  - Can have any shape, including aspherics and Zernike-based freeforms.
  - Can have a complex grooves pattern.

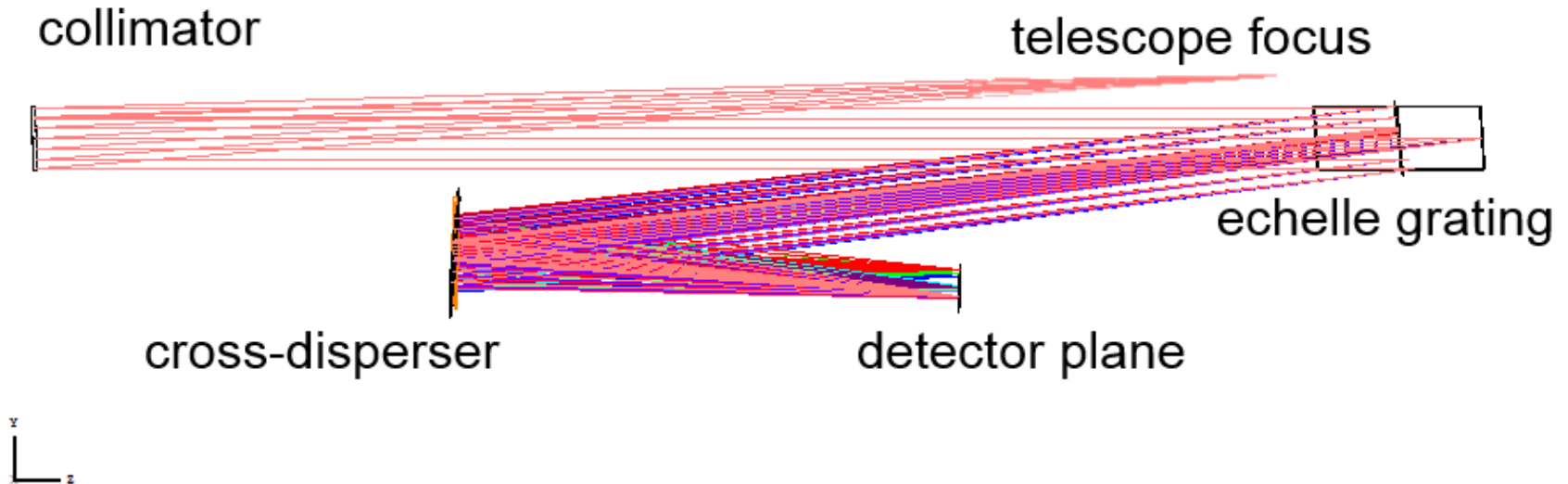


## Current baseline design concept

Parameters	Value	Comments
Collimator focal length	1939.5 mm	= Largest dimension of the instrument
Echelle grooves frequency	101 gr/mm	In the safe zone
Echelle AOI	69.436 °	In the safe zone
Orders	85-155	Feasible high-order mode
Detector format	50.8x45.1 mm	Can be single square detector
Cross-disperser grooves frequency	500 gr/mm	Manufacturable
Cross-disperser focal length	800 mm	Manufacturable
Length of the image lines		
1 <sup>st</sup>	50.84 mm	
Last	24.97 mm	
Spectral length of the orders		
1 <sup>st</sup>	<b><u>2.6 nm</u></b>	<b><u>Factor of 2 difference</u></b>
Last	<b><u>0.7 nm</u></b>	<b><u>Order of magnitude difference</u></b>



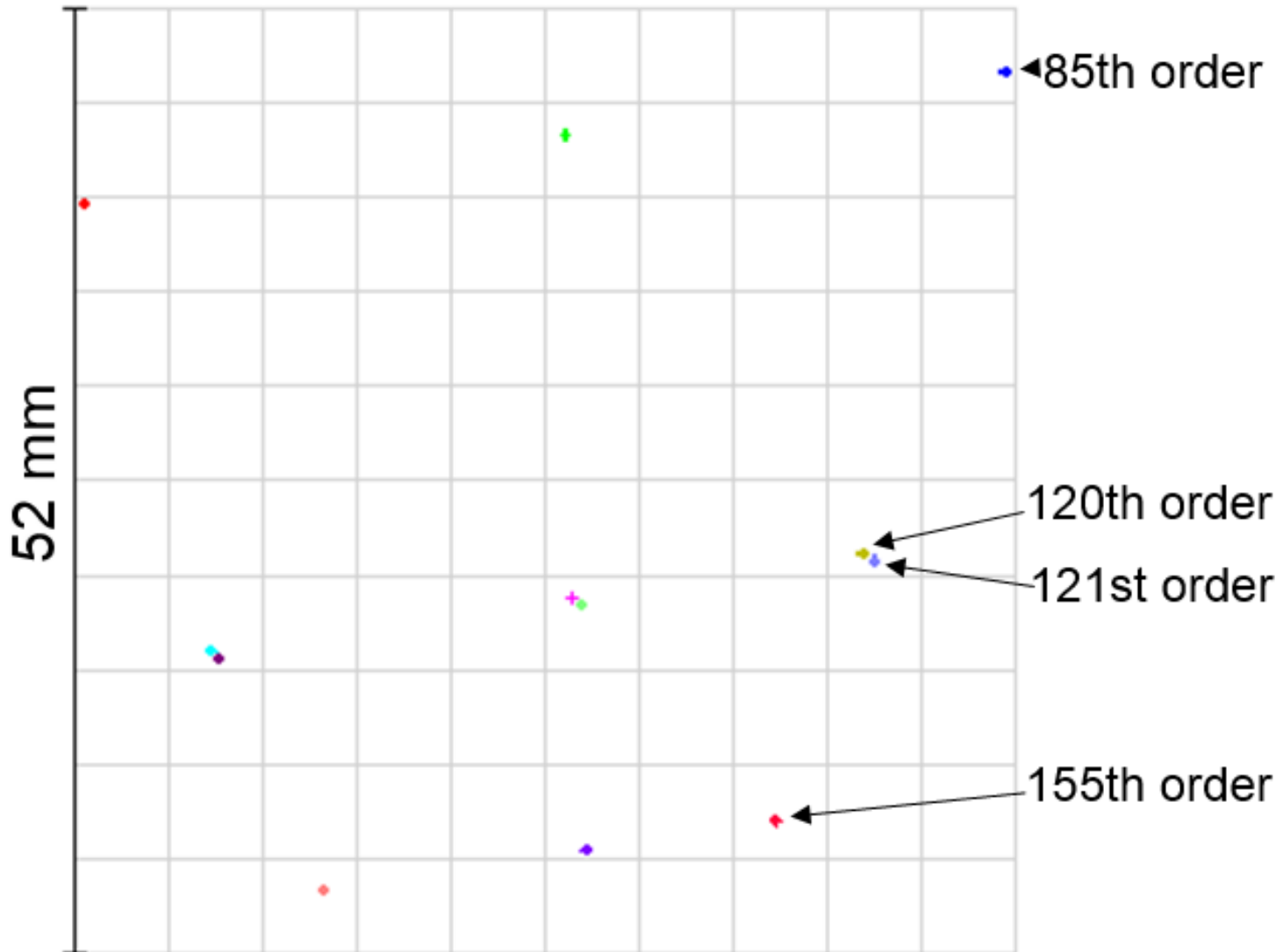
# Optical scheme



The optical scheme represents almost classical echelle spectrograph  
In a quasi-Littrow mounting with a single cross-disperser

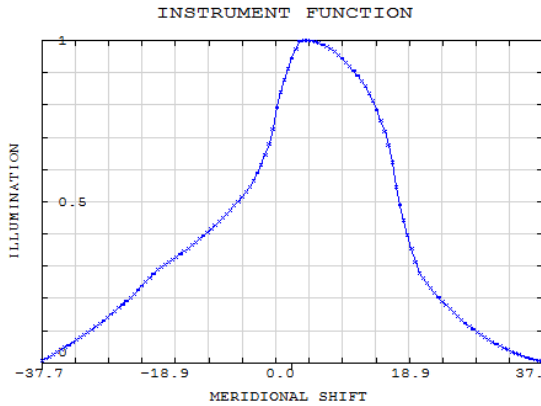


# Spectrum format

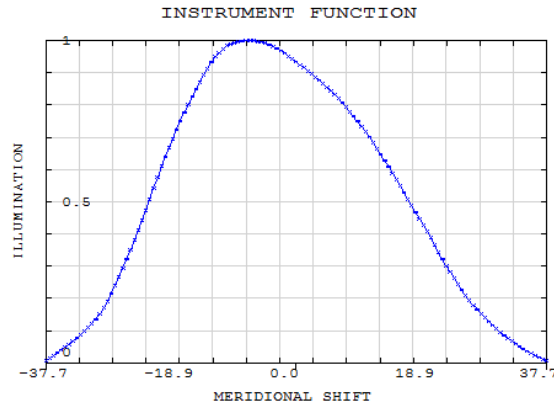




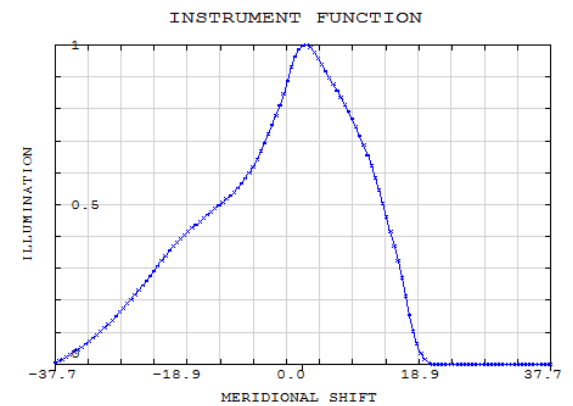
# Optical quality and resolution (I)



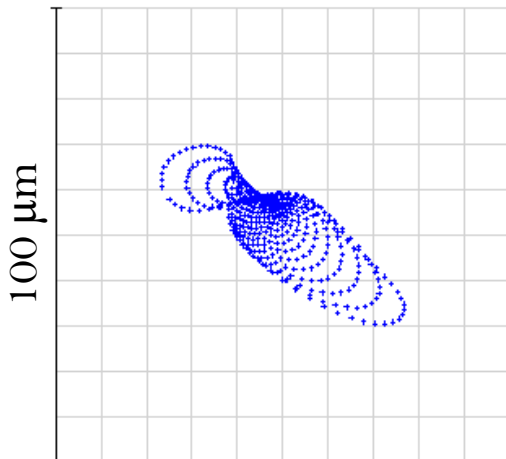
WIDTH	
ENTRANCE SLIT WIDTH, MICRONS	18.0000
FULL WIDTH ON A HALF OF THE MAX, MICRONS	24.1920
WIDTH ON LEVEL 0.1, MICRONS	57.6000



WIDTH	
ENTRANCE SLIT WIDTH, MICRONS	18.0000
FULL WIDTH ON A HALF OF THE MAX, MICRONS	39.1680
WIDTH ON LEVEL 0.1, MICRONS	61.6320

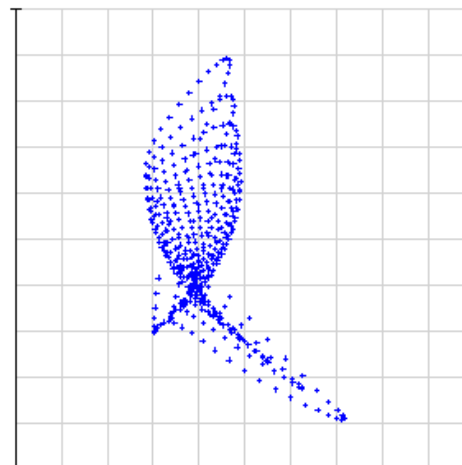


WIDTH	
ENTRANCE SLIT WIDTH, MICRONS	18.0000
FULL WIDTH ON A HALF OF THE MAX, MICRONS	24.7680
WIDTH ON LEVEL 0.1, MICRONS	47.8080



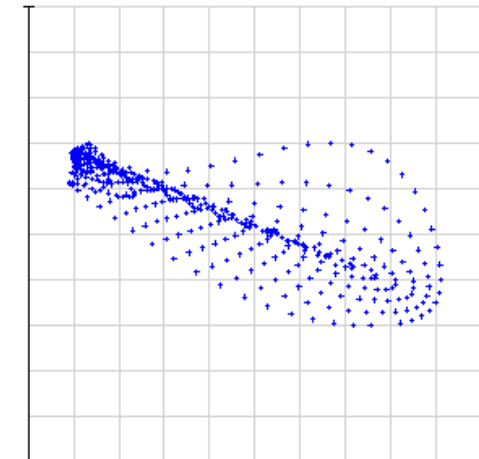
217.4 nm

IF FWHM = 24.2 μm  
Spot RMS = 27.2 μm



218.7 nm

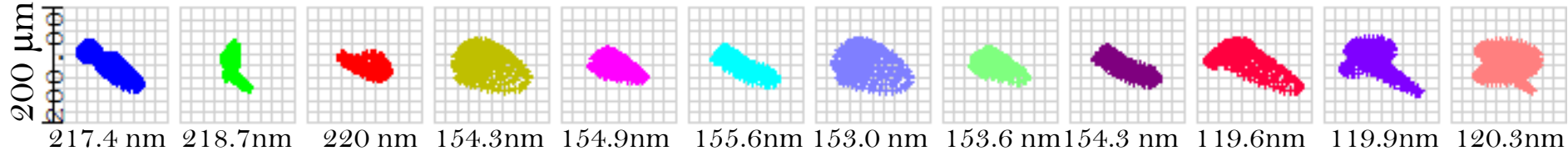
IF FWHM = 39.2 μm  
Spot RMS = 20.1 μm



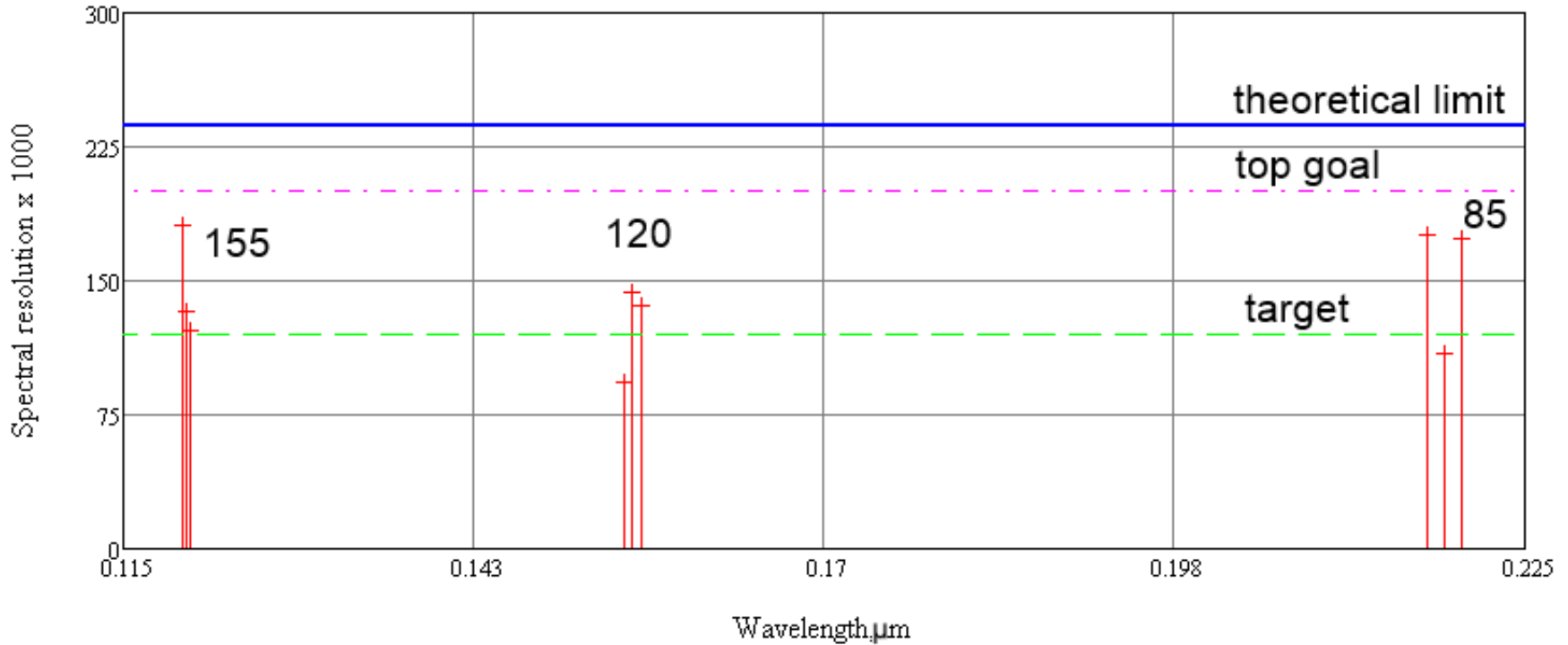
220.0 nm

IF FWHM = 24.8 μm  
Spot RMS = 30.2 μm

# Optical quality and resolution (II)

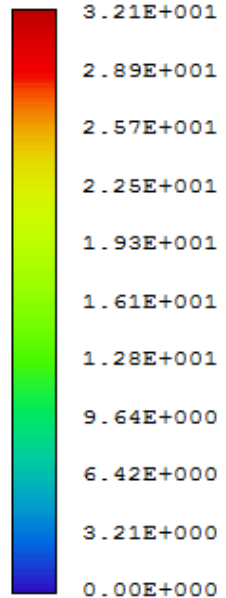
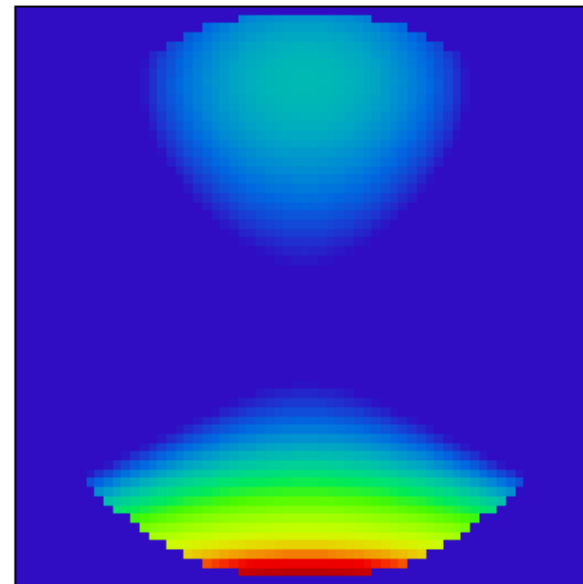
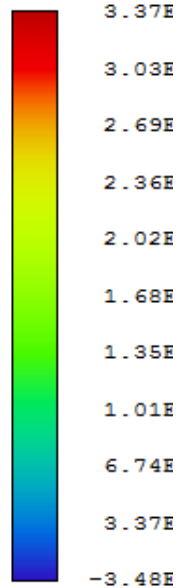
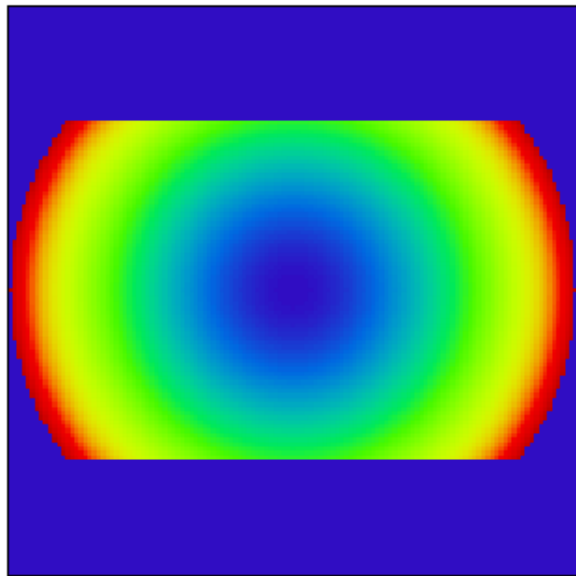


Spot diagrams for all the control wavelengths



Spectral resolution in the 85<sup>th</sup>, 120<sup>th</sup> and 155<sup>th</sup> orders vs the target values

# Notes on the cross-disperser (I)



Cross-disperser grating sag:  
Sphere R=1601.05 mm  
+Zernike modes:

V. ast 1 and 2, V. coma 1, V. tref, V. quadrof., Prim sph.

Residual after the BFS subtraction

RMS error = 6.65  $\mu\text{m}$

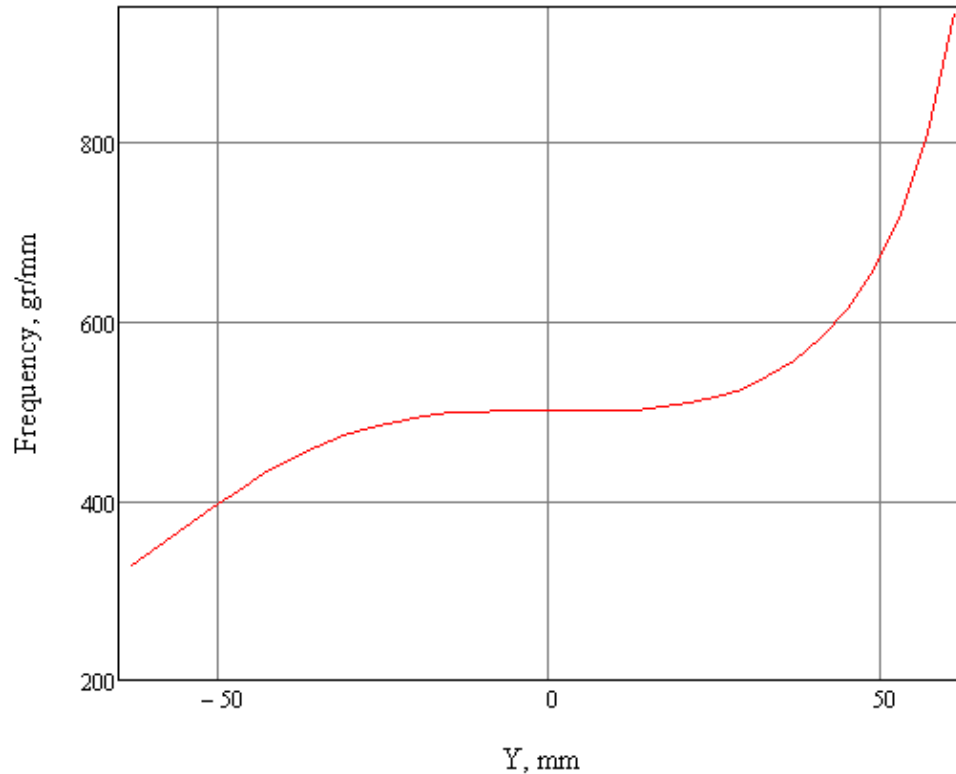
Max error = 32.12  $\mu\text{m}$



## Notes on the cross-disperser (II)

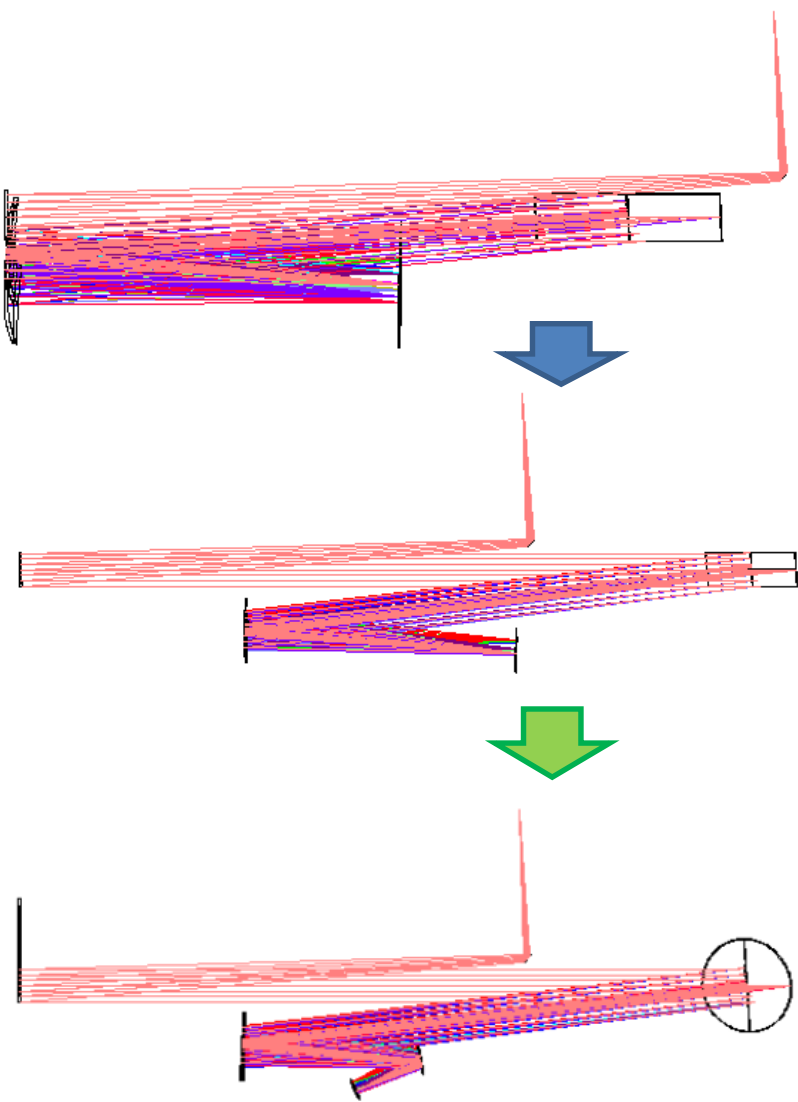
The grating has variable line spacing defined by the equation:

$$d_{eff} = \frac{1}{T} + \alpha \cdot y + \beta \cdot y^2 + \gamma \cdot y^3 + \delta \cdot y^4 + \varepsilon \cdot y^5$$



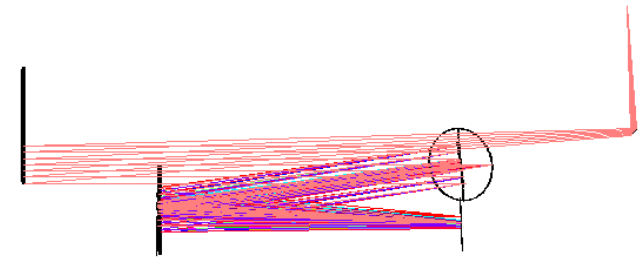
Grooves frequency vs. the Y coordinate on the cross-disperser surface

# Other configurations considered



## Scheme 0

$F_{col} = 1212 \text{ mm}$   
 $F_{cam} = 500 \text{ mm}$   
 $N_{echelle} = 229 \text{ gr/mm}$   
 Orders = 39-71  
 $d\lambda = 3.1 \text{ nm}$   
 Det. W x H  
 = 117 x 65 mm  
 FWHM ~ 31.7  $\mu\text{m}$

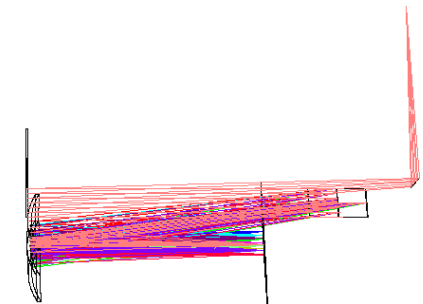


## Scheme 2e

$F_{col} = 3124 \text{ mm}$ ,  $F_{cam} = 1490 \text{ mm}$   
 $N_{echelle} = 350 \text{ gr/mm}$ , Orders = 21-27  
 Range = 179-240 nm,  $d\lambda = 6 \text{ nm}$   
 Det. W x H = 243 x 53 mm  
 FWHM ~ 32.8  $\mu\text{m}$

## Scheme 1

$F_{col} = 1939.5 \text{ mm}$   
 $F_{cam} = 800 \text{ mm}$   
 $N_{echelle} = 101 \text{ gr/mm}$   
 Orders = 85-155  
 $d\lambda = 0.7 \text{ nm}$   
 Det. W x H =  
 51 x 45 mm  
 FWHM ~ 39.2  $\mu\text{m}$



## Scheme 1m

=

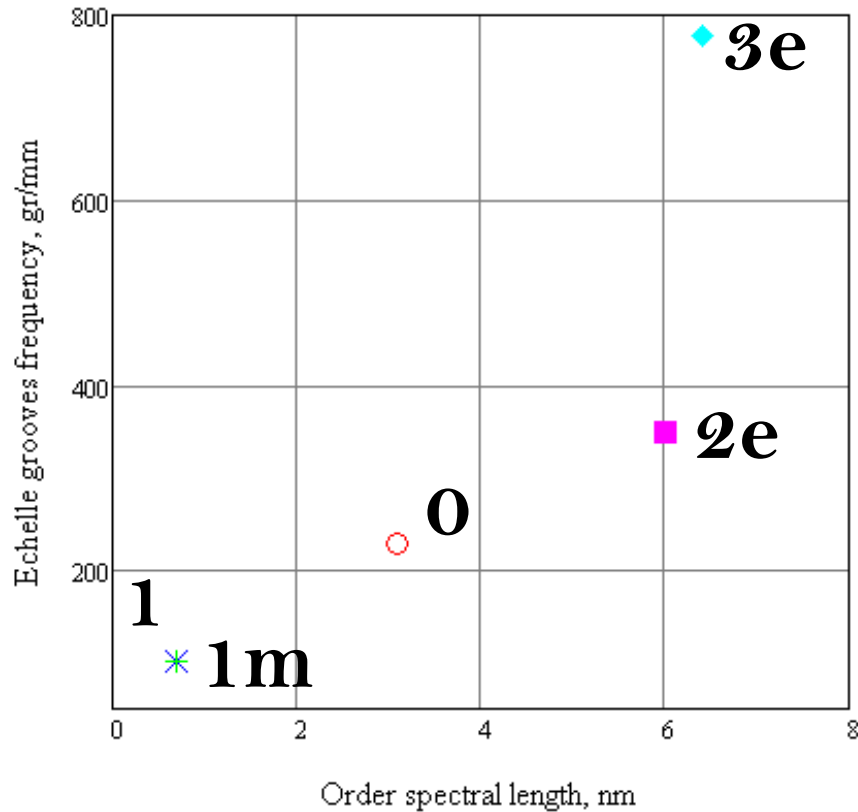
**Scheme 1+**  
**Additional**  
**mirror**

FWHM ~ 19  $\mu\text{m}$

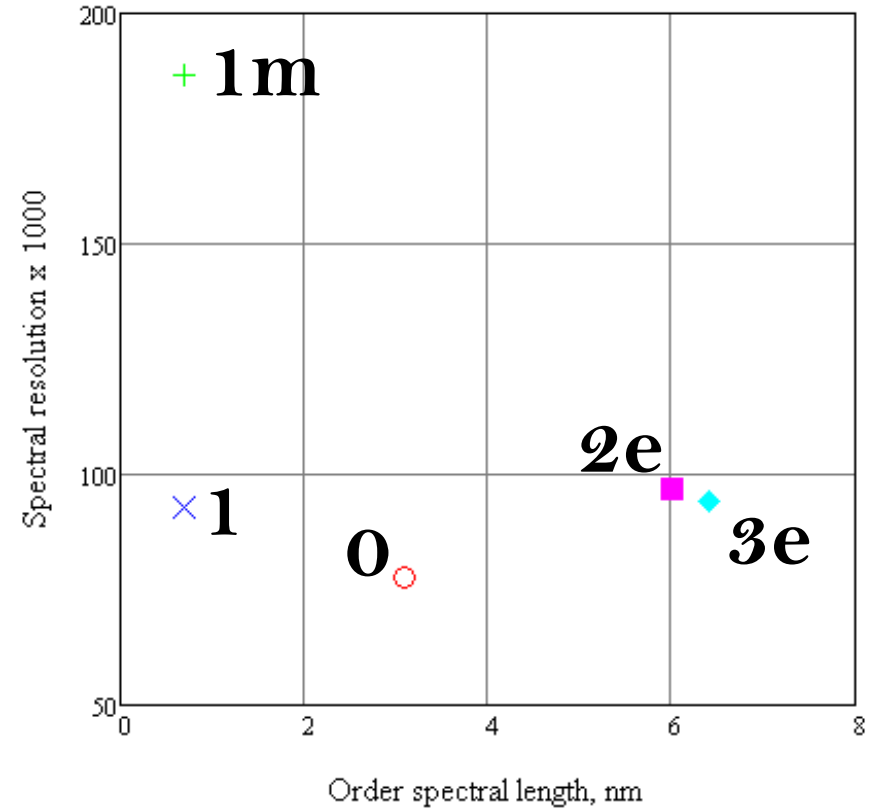
## Scheme 3e

$F_{col} = 1504 \text{ mm}$ ,  $F_{cam} = 600 \text{ mm}$   
 $N_{echelle} = 778 \text{ gr/mm}$ , Orders = 11-19  
 $d\lambda = 6.4 \text{ nm}$   
 Det. W x H = 259 x 72 mm  
 FWHM ~ 36.3  $\mu\text{m}$

## Comparison of the trial designs

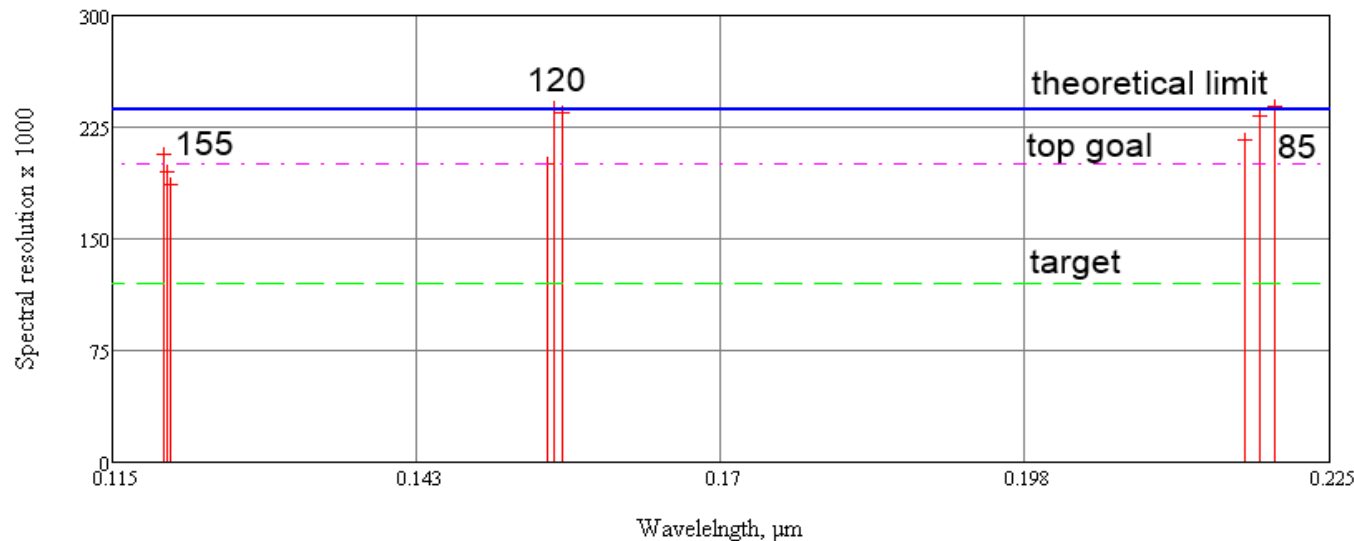
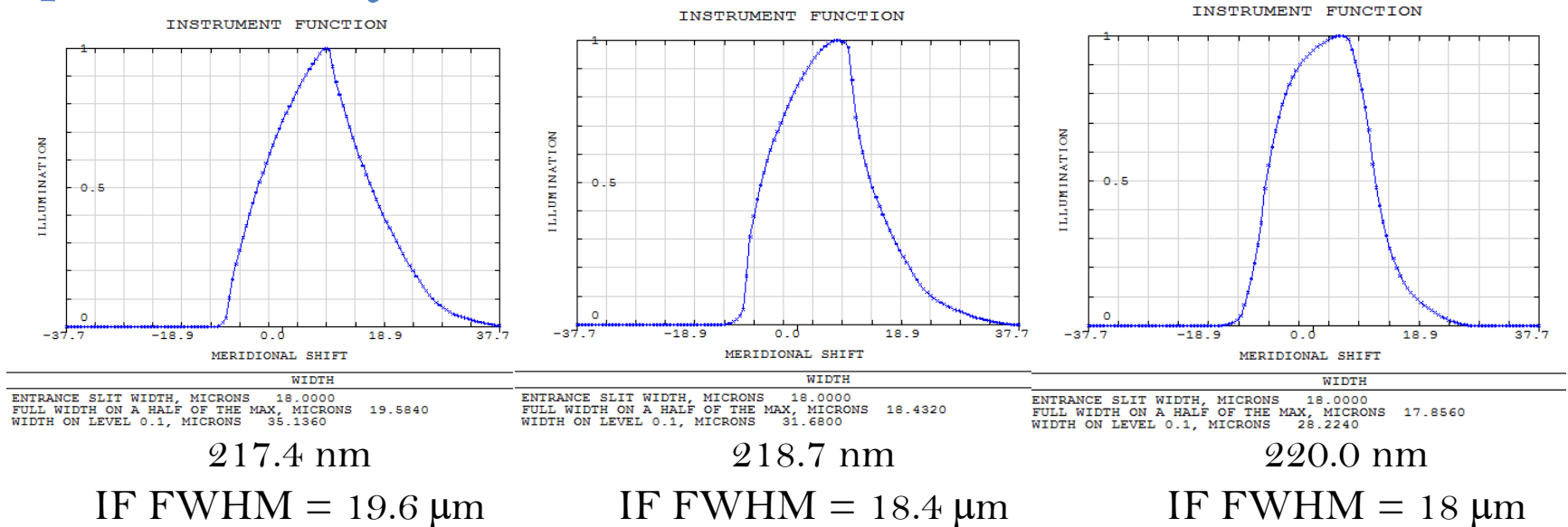


Echelle grooves frequency  
VS  
Spectral length of the shortest line  
in the spectrogram



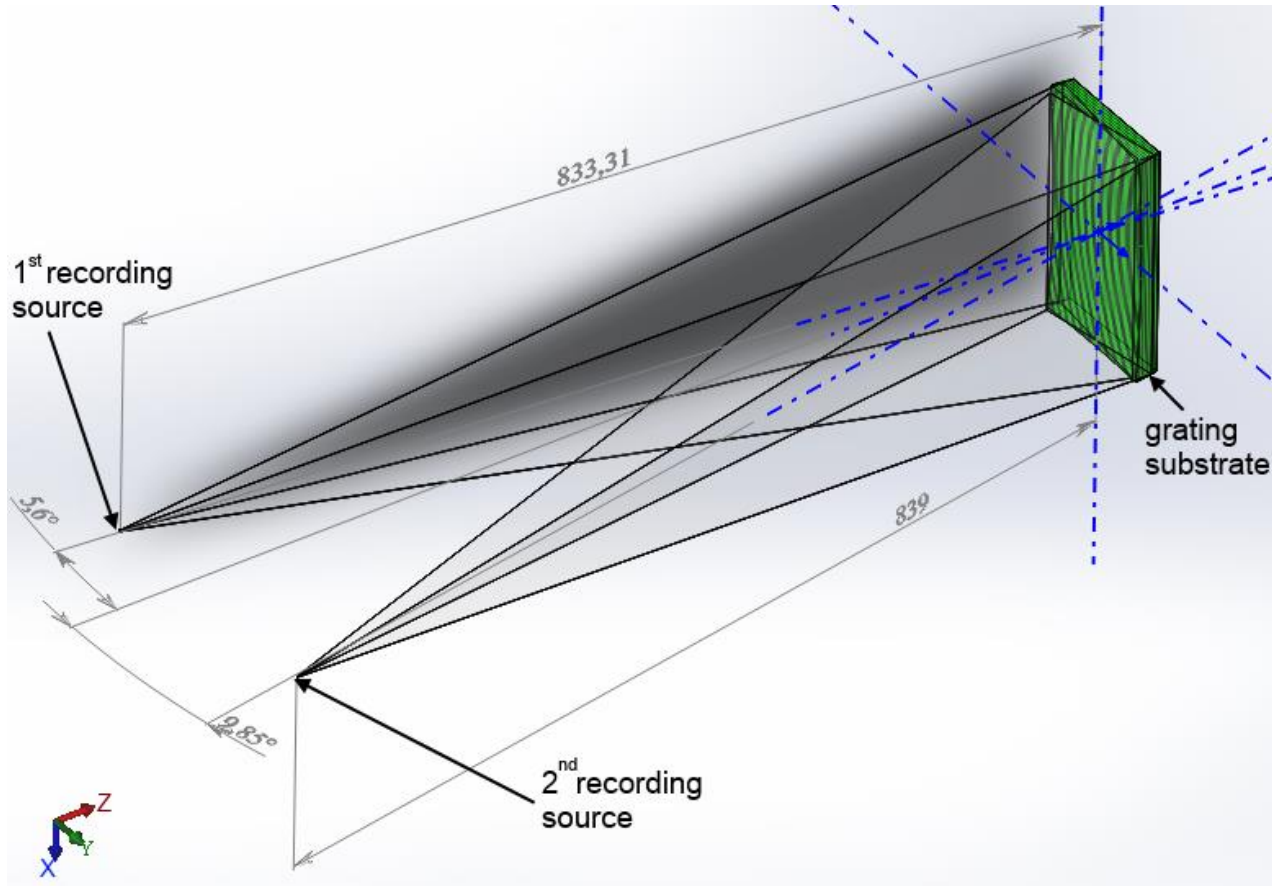
Spectral resolution for the worst point  
VS  
Spectral length of the shortest line  
in the spectrogram

# Optical quality and resolution with additional mirror

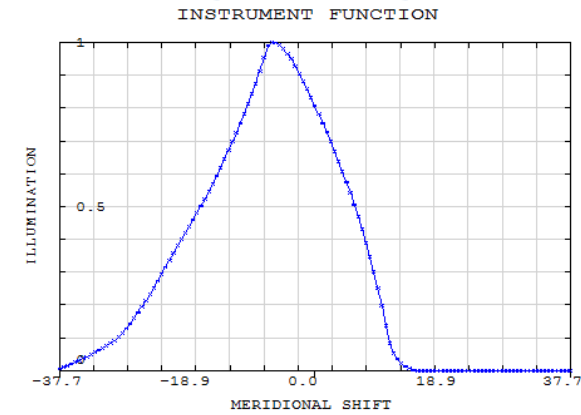


Spectral resolution in the 85<sup>th</sup>, 120<sup>th</sup> and 155<sup>th</sup> orders vs the target values

# Possible implementation of the cross-disperser grating

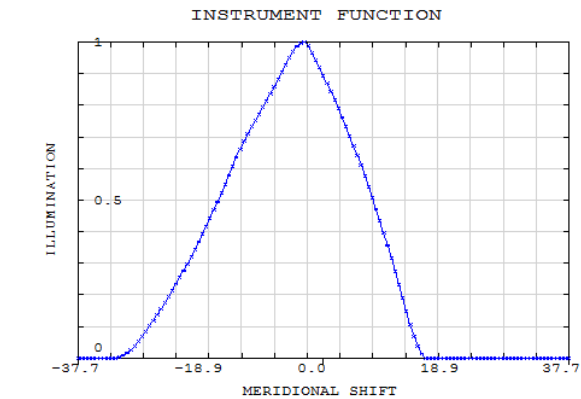


The holographic grating recording scheme:  
The two sources are points emitting @ 532 nm.



WIDTH	
ENTRANCE SLIT WIDTH, MICRONS	18.0000
FULL WIDTH ON A HALF OF THE MAX, MICRONS	23.0400
WIDTH ON LEVEL 0.1, MICRONS	39.7440

IF @ 120.3 nm with VLS grating  
IF FWHM = 23  $\mu\text{m}$



WIDTH	
ENTRANCE SLIT WIDTH, MICRONS	18.0000
FULL WIDTH ON A HALF OF THE MAX, MICRONS	23.6160
WIDTH ON LEVEL 0.1, MICRONS	40.3200

IF @ 120.3 nm with hologr. grating  
IF FWHM = 23.6  $\mu\text{m}$





## Conclusions and open questions

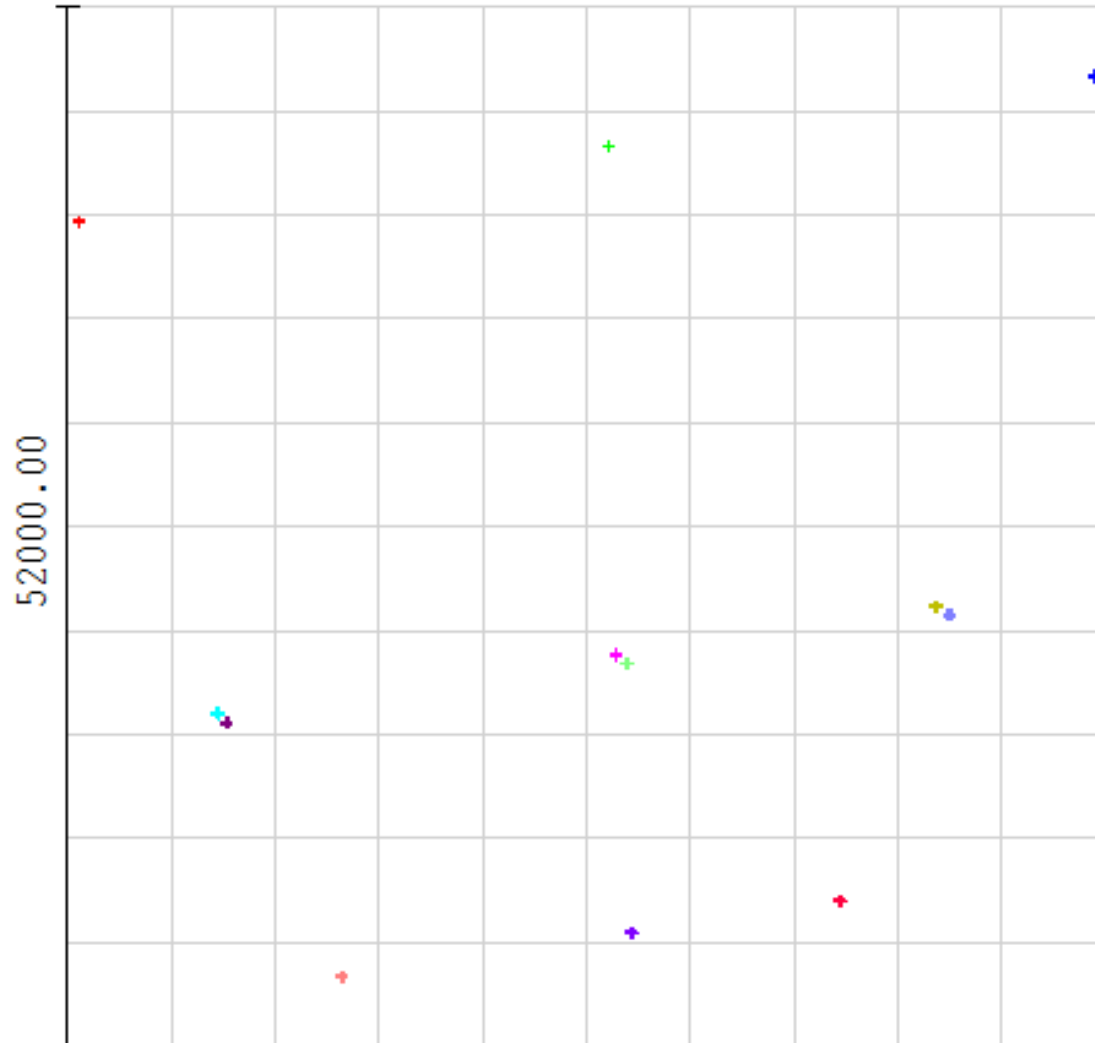
### ➤ **Conclusions on the optical design**

- The most of the requirements can be met with the current baseline design concept
- The critical requirement is the spectral length of the shortest order
- All the design parameters can be within the current or expected technological limits

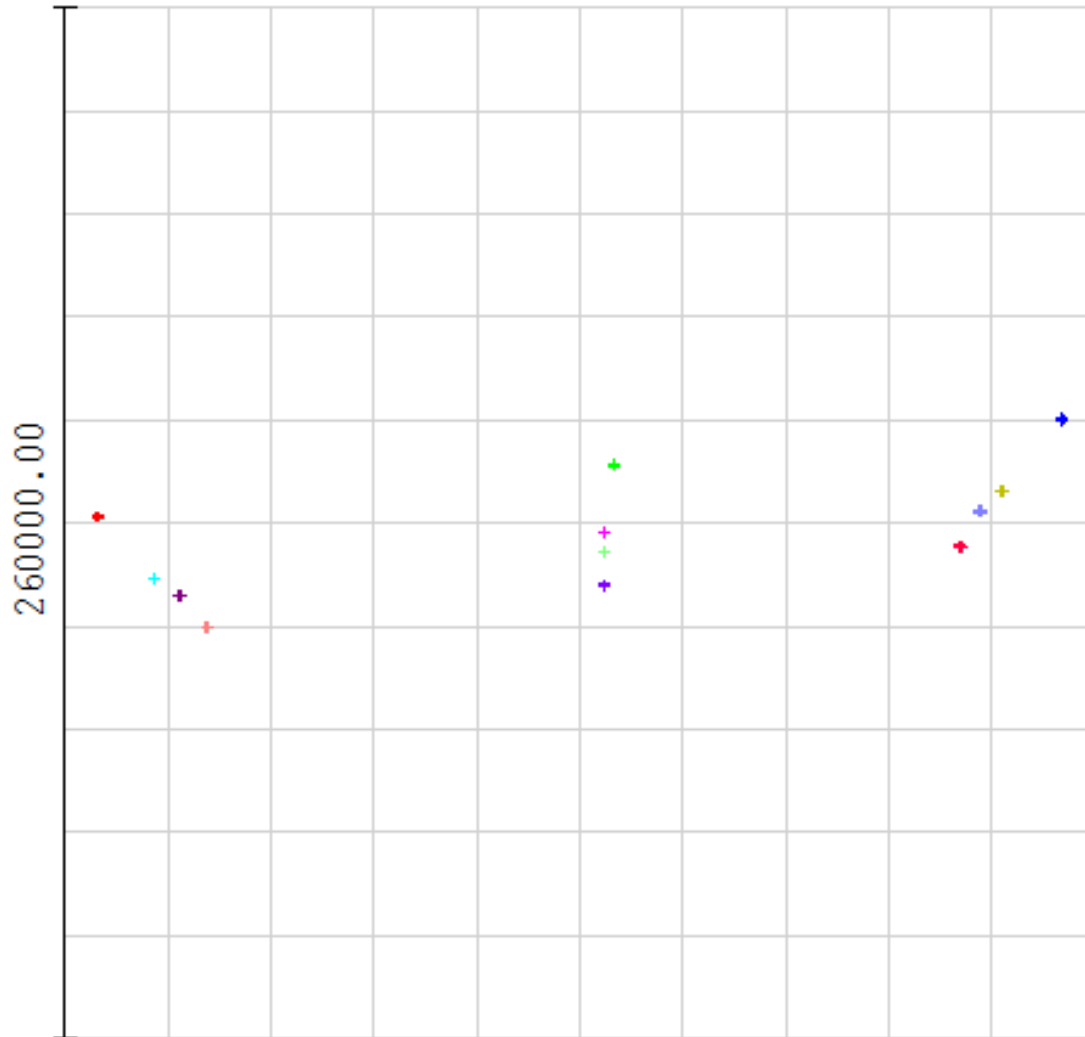


**THANK YOU FOR YOUR ATTENTION!**

## Design 1 and 1e – detector format

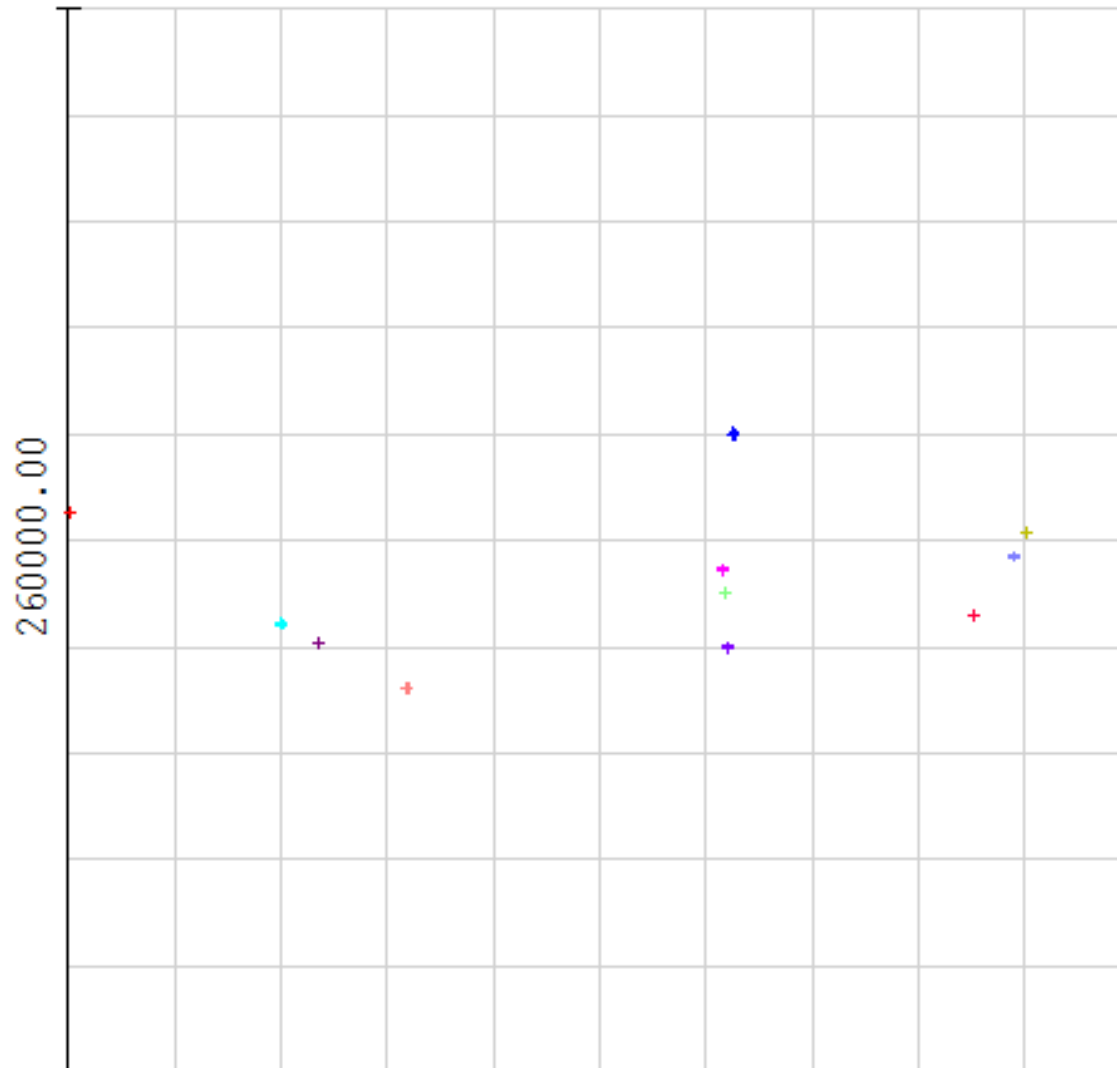


## Design 2e – detector format



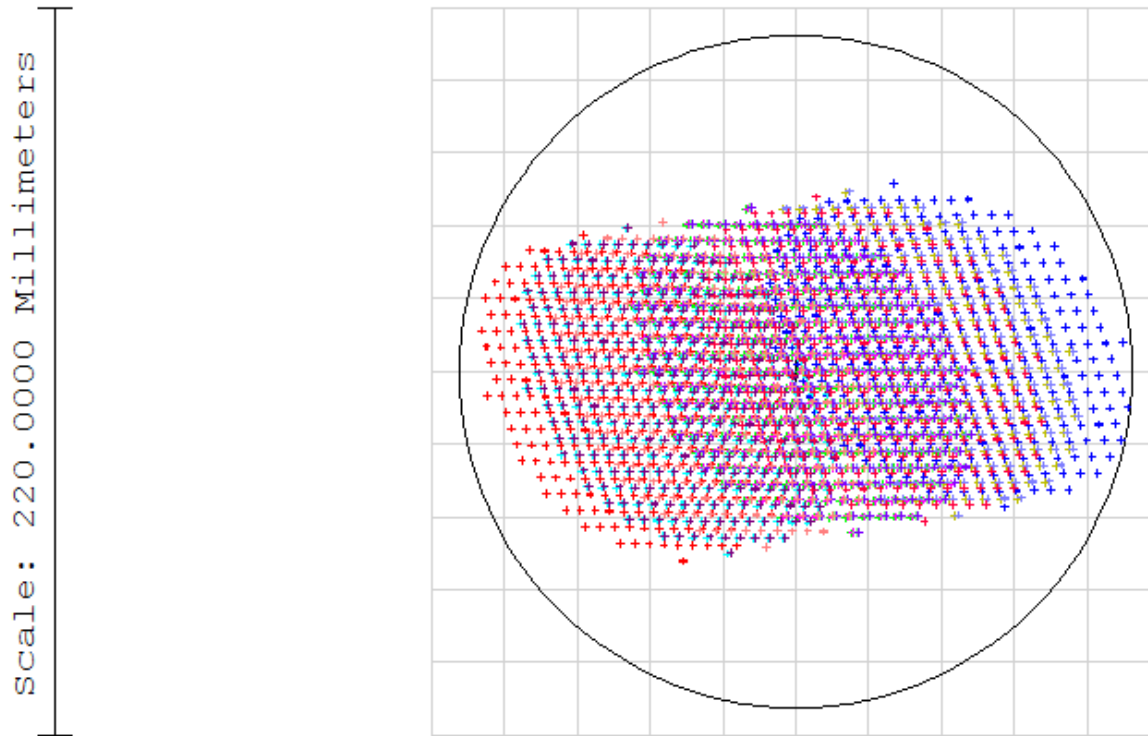


## Design 3e – detector format





## Design 1 and 1m – footprint on the cross-disperser



Aperture Diameter: 203.2593

% rays through = 100.00%

### Footprint Diagram

21.03.2017

Surface 16: cross disp

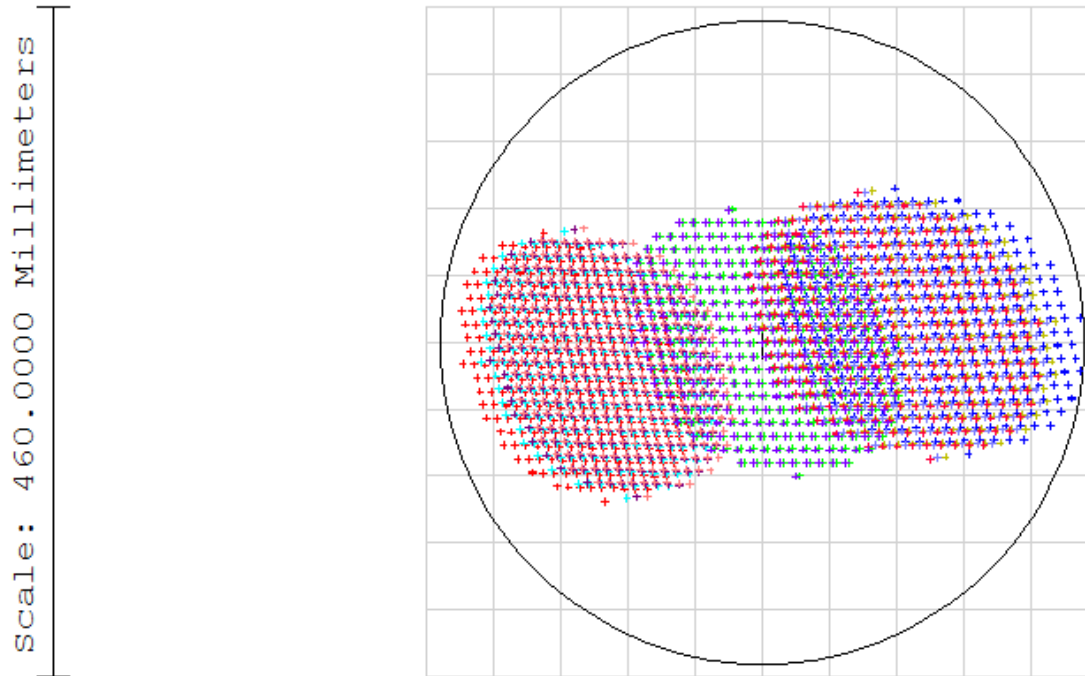
Ray X Min = -94.9471 Ray X Max = 100.1646

Ray Y Min = -57.3711 Ray Y Max = 56.5782

Max Radius= 100.7688 Wavelength= 0.1203

echelle 100-200+2 ell1 1000 mm v2.1 100 gr mm.ZMX  
Configuration: All 12

## Design 2e – footprint on the cross-disperser



Aperture Diameter: 442.2392

% rays through = 100.00%

### Footprint Diagram

21.03.2017

Surface 16: cross disp

Ray X Min = -206.3103 Ray X Max = 217.9511

Ray Y Min = -109.3438 Ray Y Max = 105.7494

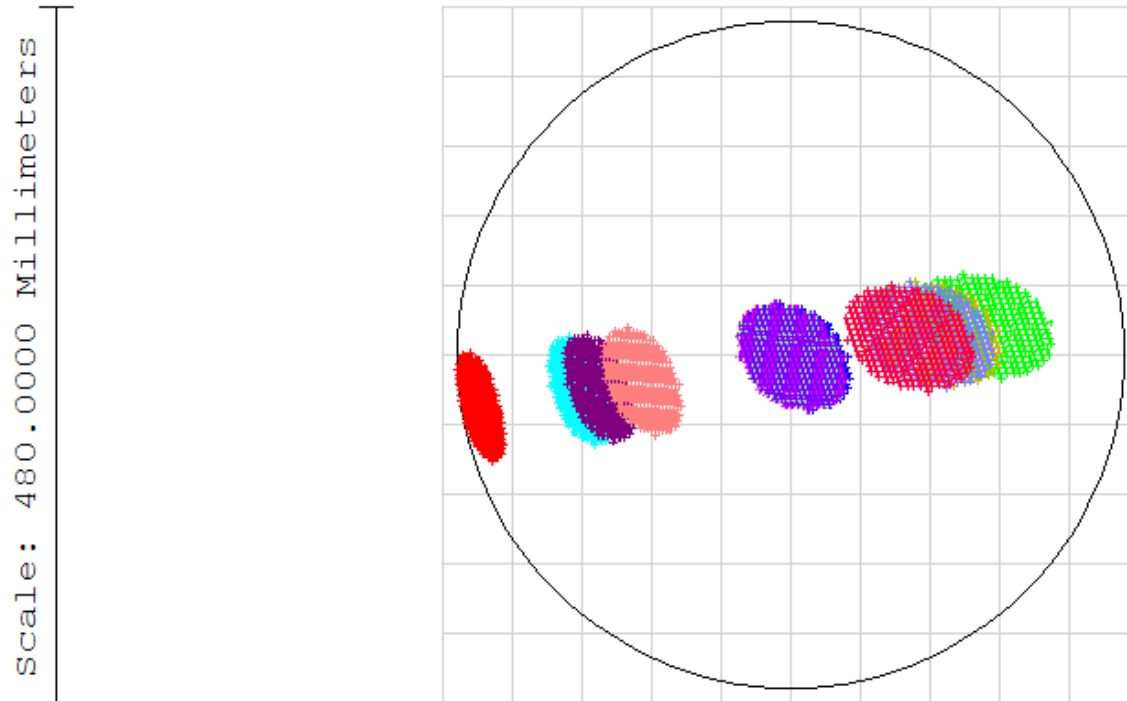
Max Radius= 218.8040 Wavelength= 0.1858

echelle 100-200+2 e111 1000 nm v2.1 how many channels.unx

Configuration: All 12



## Design 3e – footprint on the cross-disperser



Aperture Diameter: 459.7113

% rays through = 100.00%

### Footprint Diagram

21.03.2017

Surface 16: cross disp

Ray X Min = -229.2177 Ray X Max = 179.3505

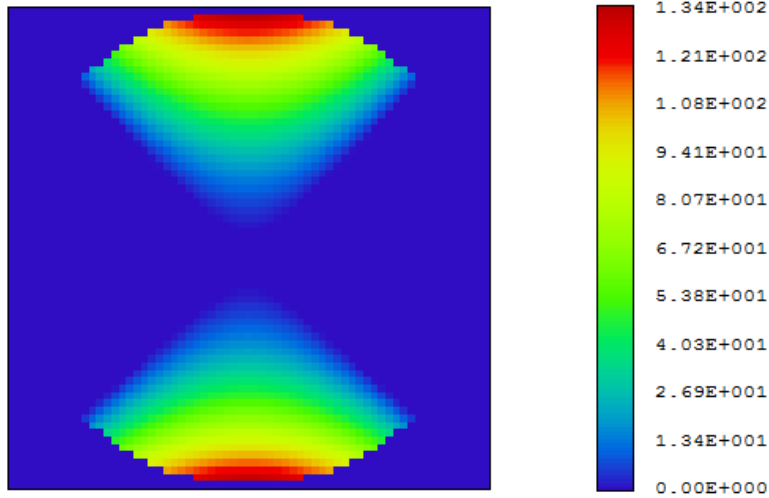
Ray Y Min = -73.5390 Ray Y Max = 55.6866

Max Radius= 229.8610 Wavelength= 0.1252

echelle 100-200+2 ell1 1000 mm v2.1 6nm.ZMX  
Configuration: All 12



# Design 1m – freeforms shapes

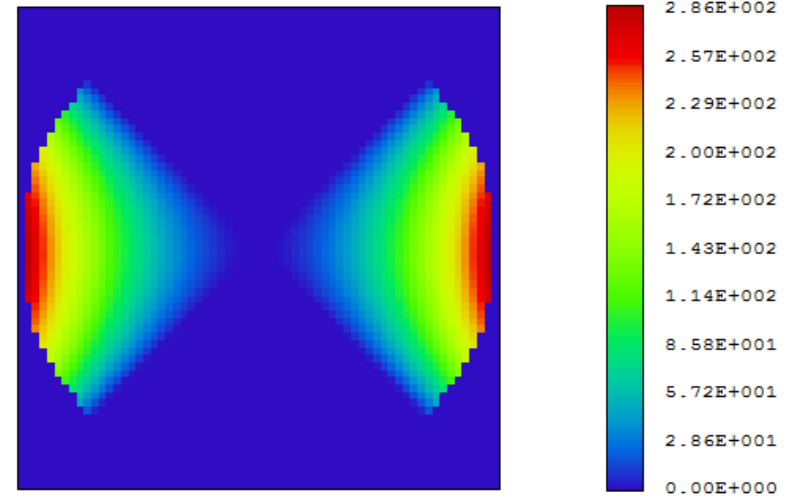


Fitting\_results

03.04.2017  
BFS Radius RR=1537.7052mm  
Center displacement C=0.0009mm  
RMS\_ERROR=45.4064microns  
MAX\_ERROR=134.4990microns

echelle 100-200x2 ell11 1000 m v0.1 100 gr mm+mirror.nxx  
Configuration "12" of 12

Grating



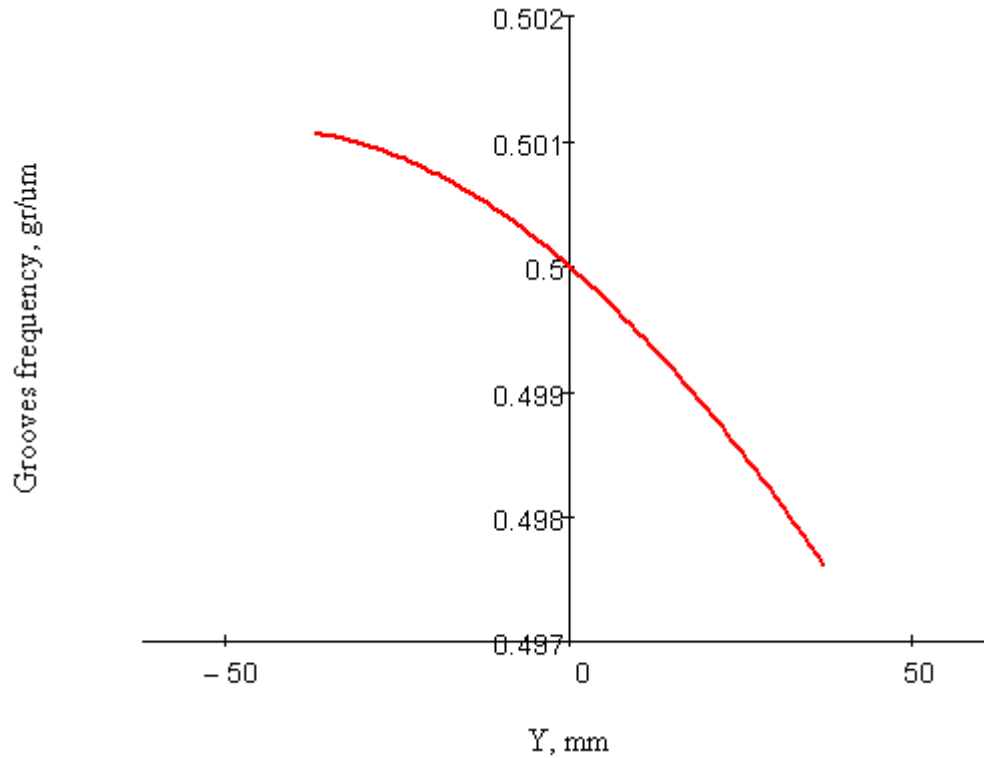
Fitting\_results

03.04.2017  
BFS Radius RR=-5284.8849mm  
Center displacement C=-0.0002mm  
RMS\_ERROR=97.8477microns  
MAX\_ERROR=-287.2402microns

echelle 100-200x2 ell11 1000 m v0.1 100 gr mm+mirror.nxx  
Configuration "12" of 12

Mirror

## Design 1m – VLS grating



Cross-disperser grating frequency law